

A non-drag-free gravitational-wave mission architecture

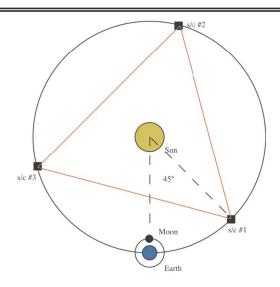
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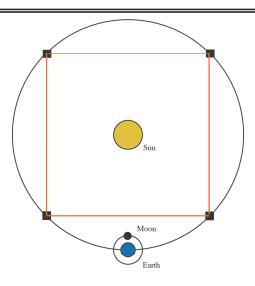
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#1: Which concept should be studied? Triangle or square?





- The cost of 3 dual-string spacecraft with 6 telescopes/instruments should cost about the same as 4 single-string spacecraft with 8 telescopes/instruments
- For purposes of response to the RFI request for cost, mass, etc estimates based on on engineering work, analogies to the GRAIL mission with 2 single-string spacecraft recently launched will be more credible than creating a 3-spacecraft mission from thin air.
- Because the cost of the payload is the largest unknown, if a Team-X study is undertaken a study of the 3 spacecraft option is recommended



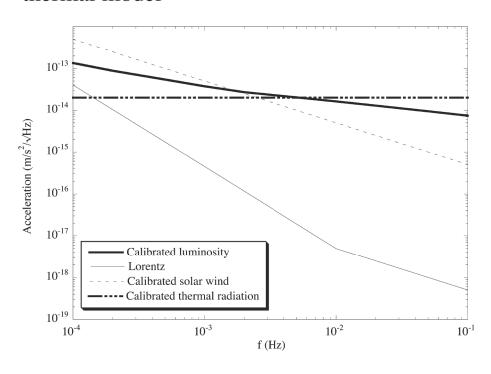
#2: Would the Disturbance Free Payload described in the RFI By Shao, et al. be applicable to this concept?

• No. The Shao et al. concept includes a drag-free system, albeit with possibly coarser control, but that spacecraft positions control is counter to the non-drag-free approach where NO thrusting is used during science operations.



#3: Without drag-free, the noise budget is sensitive to noisy forces and mechanical disturbances on the spacecraft that are difficult to rule out on the ground and measure/model in space (e.g. Pioneer Anomaly). Are these controllable? What is the budget for unmodeled forces?

- Noise budget needs to be done for any GW mission
- Leading terms are discussed in paper, but more work needs to be done
- Unknown forces cannot be modeled, so there is always some risk;
 - A drag-free sensor has similar risks
- Note that there is good evidence that 'Pioneer anomaly' is well explained by spacecraft thermal model



Solar calibrated to voltage standard noise
Solar wind calibrated to 1%
Solar panel temperature controlled to 0.1 mK
(and assumes Earth environment (GRAC)
Lorentz force based on 30 V potential

Not shown are:

Surface outgassing Thruster leakage



#4: Do you have an estimate of what delta-v is required for each spacecraft and how long the cruise phase will last?

- A simple calculation for a 3.5 year transit time to 180 degrees from Earth gives delta-v required = 2*1.43 km/s
 - one maneuver of 1.43 km/s at launch to reduce orbit period to 7/8 year, and similar maneuver to circularize
- Taking spacecraft mass of 350 kg, using Hall thruster (Busek BHT-600) with 42 mN thrust, Isp 1585 s, then 138 days of thrusting is required for each maneuver
- Total propellant mass is 65 kg
- GRAIL spacecraft dry mass is 200 kg, propellant mass is 100 kg
 - Assume non-drag-free spacecraft mass is 250 kg, 64 kg propellant mass, leaving 36 kg.
- GRAIL spacecraft peak power is 700 W



#5: What comm. capability is required? What antenna sizes are required onboard and at the ground station? Would you consider lower sampling because of the lower frequency response?

- 1.25 m spacecraft antenna using X-band with 17 W transmitted power to a DSN 34m antenna gives a data rate > 15,000 bits/second
 - Antenna field of view is sufficient to see Earth at all times with no articulation
- Suggested data rate is 1500 bits/second, 130 Mb/day
 - -2.5 hours of contact per day (or 7.5 hours every third day) would get data down
- This data rate based on 2000 ESA Final Technical Report
 - LISA sensitivity might be achievable with larger telescope or shorter wavelength laser,
 so assume same interferometer data rate
 - Limited at low frequencies by binary confusion noise
 - No drag free sensor or control system, but similar data volume assumed for solar pressure, thermal, solar wind. etc. calibration data



Simple telemetry link calculation

| RF Power, dBm | 42.30 | | | | | | |
|------------------------------|----------|----------|---|----------|----|--|--|
| (Watts) | | 17.00 | | | | | |
| Transmit Circuit Loss, dB | -1.00 | | 1 is typical conservative value | | | | |
| Antenna Circuit Loss, dB | -0.50 | | .5 is typical conservative value | | | | |
| Antenna Gain, dBi | 38.24 | | | | | | |
| Antenna diameter, m | | 1.25 | | | | | |
| Wavelength, cm | | 3.40 | 3.4 cm | is X-bar | nd | | |
| Efficiency | | 0.50 | 0.5 is typical | | | | |
| Pointing Error, dB | -1.00 | | related to how far off beam center | | | | |
| Total: | 78.05 | | | | | | |
| th Parameters: | | | | | | | |
| Space Loss, dB | -280.90 | | | | | | |
| Range, km | | 3.00E+08 | | | | | |
| Atmospheric Atten, dB | -0.50 | | | | | | |
| Total: | -281.40 | | | | | | |
| ceiver Parameters: | | | | | | | |
| Polarization Loss, dB | -0.50 | | | | | | |
| Antenna Gain, dBi | 68.39 | | | | | | |
| Antenna diameter, m | | 34.00 | | | | | |
| Efficiency | | 0.70 | | | | | |
| Pointing Loss, dB | -1.00 | | | | | | |
| Noise Spectral Dens, dBm/Hz | -183.83 | | | | | | |
| System Temp, K | | 30.00 | | | | | |
| wer Summary: | | | | | | | |
| Received Power, dBm | -136.46 | | | | | | |
| Received Pt/N0, dB-Hz | 47.37 | | | | | | |
| SNRV(1-sec) | 330.49 | | | | | | |
| lemetry: | | | | | | | |
| Bit Rate, dB-Hz | 44.77 | | | | | | |
| Bit Rate, bps | 30000.00 | | Really Symbol rate, typically 2* (information rate) | | | | |
| Data Power / Total Power, dE | 0.00 | | | | | | |
| Tlm Mod Index, deg | 90.00 | | | | | | |
| TLM Rcvr Losses, dB | 0.00 | | | | | | |
| Eb/NO, dB | 2.60 | | Symbol margin, needs to be >2 typically | | | | |



6: Do you have an estimate of the total launch mass, and a candidate launch vehicle?

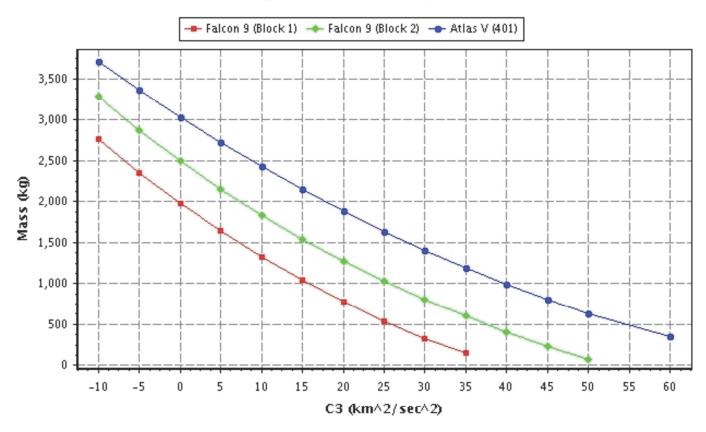
- Assume single-string spacecraft launch mass = 350 kg
 - GRAIL spacecraft dry mass = 200 kg
 - Additional payload mass = 35 kg
 - Propellant = 65 kg
 - Contingency = 50 kg
- Mass of 4 single-string spacecraft = 1400 kg
- Mass of launch adaptors (2x GRAIL) = 300 kg
- Launch mass 1700kg + margin
- For launch to $C3 \sim 1 \text{ km}^2/\text{s}^2$, Falcon-9 block -2 or Atlas V-401 would work
 - − Falcon 9 Block 2 launches ~2400 kg to C3 ~1
 - Atlas V 401 launces ~2900 kg to C3 ~1
- With 3 dual-string spacecraft Falcon-9 Block 1 might suffice
 - Falcon-9 block 1 launches \sim 1900 kg to C3 \sim 1



Launch vehicle performance data

- From NASA launch services web site
- http://elvperf.ksc.nasa.gov

NASA ELV Performance Estimation Curve(s) High Energy Orbits Please note ground rules and assumptions below.





7: Where do the cost savings come over the SGO-Mid concept?

- SGO-Mid requires drag-free sensor and micro-newton thrusters
 - If LISA Pathfinder is successful, and NASA mission acquires GRS from Europe, GRS cost might cost \$50M-\$100M, and thruster development might cost >\$10M
 - If NASA mission does not use Pathfinder contractors, or Pathfinder is not successful, then development of NASA drag-free system might require a flight demonstration, so cost could be very high.
- Other than GRS, the non-drag-free system reduces number of actuators, complexity of interferometry, demanding requirements on spacecraft
 - Team-X study not likely to correctly reflect cost of meeting drag-free requirements

| Assembly | SGO-Mid | Non-Drag-Free |
|----------------------|---------|---------------|
| Point ahead actuator | Yes | No |
| IFO back-link | Yes | No |
| Stablity requirement | 50 pm > | 1 nm |
| S/C Mass balance | Yes | No |
| Telecon steering | Yes | No |
| GRS | Yes | No |
| "N thrusters | Yes | No |